

1                                   **HEAD GIMBAL ASSEMBLY METHOD**

2                   The present application is a continuation of United States Provisional  
3                   Patent Application Serial Number 60/102,860, for Method for Manufacturing a  
4                   Head Gimbal Assembly, filed October 2, 1998, the specification of which in  
5                   incorporated herein in its entirety.

6                                   **FIELD OF THE INVENTION**

7                   The present invention relates generally to assembly procedures used in the  
8                   manufacture of hard disk drives and particularly to a method of assembling a head  
9                   gimbal assembly and testing procedures used in evaluating the assembled  
10                  component parts of the head gimbal assembly at various stages in the assembly  
11                  process.

12                                  **BACKGROUND OF THE PRESENT INVENTION**

13                  The hard disk drive is the principal device used for long term, bulk  
14                  memory storage in today's computers. The hard disk drive includes a rotating  
15                  disk and a head gimbal assembly that is attached to actuator arm in the disk drive  
16                  and that is held thereby closely adjacent to the rotating disk. The head gimbal  
17                  assembly consists of several distinct components including a suspension, a

1 gimbal, a flex circuit, and a slider with its integral read/write head. The rotating  
2 disk is coated with a magnetic or read/write media that is selectively magnetized  
3 by a read/write head to store information thereon. In operation, an electric current  
4 is provided to the read/write head, which creates and applies a magnetic field to  
5 the disk as the disk rotates relative to the head. The current is selectively  
6 controlled such that the applied magnetic field selectively reverses, thereby  
7 preferentially magnetizing elective areas of the disk. Each magnetized area  
8 consists of a north and south pole selectively oriented in one of two preferred  
9 directions. Magnetized areas having a north pole pointing in one of the two  
10 direction are designated as a "0" and in the other direction as a "1." In this way the  
11 binary language of computers consisting of zeroes and ones is assembled and data  
12 and programs, which comprise zeroes and ones in binary computer language, are  
13 stored on the hard disk. To read the information, current read/write heads sense  
14 changes in the current flowing through the head as the magnetized areas of the  
15 disk pass by and recognizes the current changes as a 0 or 1.

16 Typical hard disk drives include multiple disks and multiple read/write  
17 heads. As the disks rotate in the disk drive, air flow from the spinning disks  
18 interacts with the bearing surface on the slider to create an air bearing, which is  
19 used to place the read/write head at the designed distance from the disk media,

1 also known as the hard disk drive's magnetic spacing. If the head is too far away  
2 from the media, signal loss will occur and if the head is too close to the media, the  
3 head could mechanically crash, that is, actually come into contact with the disk,  
4 resulting in damage to the head or the media and often a complete hard drive  
5 failure.

6 Currently, the hard disk drive industry is striving to increase the amount of  
7 data or information that can be stored in a predetermined area. That is, the  
8 industry is trying to increase the quantity of information stored per unit area of the  
9 disk. To do this, the magnetized disk media areas, which are representative of the  
10 stored data, must be smaller and closer together. In turn, this requires that the  
11 sliders as well as the magnetic spacing be smaller. As the sliders are made  
12 smaller, they become increasingly sensitive to factors causing spacing variation.  
13 The key mechanical factors that determine the proper magnetic spacing are the  
14 bearing manufacturing tolerances, the load placed on the slider from the  
15 suspension, and the torque acting on the slider from the suspension and assembly  
16 tolerances.

17 The performance of the read/write head is critical to the long-term  
18 operation of a hard drive. These devices include small component parts operating  
19 under extreme conditions. Precision manufacturing and quality control testing of

1 these parts prior to their incorporation into the finished hard disk drive is therefore  
2 desirable to ensure that only quality components make it into the disk drives  
3 before being sold to the consumer.

4 One of the critical components in the hard disk drive is the head gimbal  
5 assembly. The head gimbal assembly has traditionally been assembled together  
6 by hand in several steps. Presently, a head gimbal assembly process includes,  
7 broadly stated, steps including the adhesive attachment of a slider to a suspension,  
8 the routing of leads to electrically connect the head to the disk drive electronics,  
9 and the testing the electrical performance of the head while the suspension holds it  
10 over a test disk. Many problems are encountered with the present process  
11 resulting in high costs and poor magnetic spacing tolerances.

12 One of the problems is that the present system is labor intensive. This  
13 creates many potential opportunities for the generation of electrostatic charges,  
14 which can damage the components with an electrostatic discharge (ESD) or  
15 electrical overstress (EOS).

16 Another example of a problem relates to the electrical connection made  
17 between the head termination pads on the slider and the electrical interconnect or  
18 flex circuit running along the suspension after the slider is attached to the  
19 suspension. These electrical connections are difficult to make for several reasons.

1 For example, the slider is positioned with respect to the gimbal load point and not  
2 necessarily the electrical leads on the suspension, which can cause the electrical  
3 connection to be difficult and unreliable. In addition, because the intricate surface  
4 features of the head/slider and suspension make it difficult to hold in a fixture, the  
5 bonding process, which requires a significant force to achieve a good bond, often  
6 leads to damage of the suspension.

7 After attachment of the slider to the suspension, each head is tested while  
8 the suspension holds the slider over a rotating testing disk. This test is known as a  
9 dynamic electrical test (DET). Current DET test procedures require that the head  
10 gimbal assembly be held in the loaded position at the correct magnetic spacing or  
11 Z-height with respect to the spinning testing disk, making both loading the  
12 assembly and automating this test difficult. In addition, mechanical and head  
13 tolerances can cause a poor signal, making it difficult to discern the source of any  
14 poor performance. Further, the DET results indicate that a head is bad and must  
15 be discarded, then the manufacturer must throw away not only the head/slider but  
16 also the suspension to which it is bonded. This is a source for significant yield  
17 cost.

18 Static angles are currently measured with the suspension clamped and held  
19 in its loaded state, by lifting the beam with a pin near its center. While the slider

1 bond pad is the point of interest, it is impossible to load it and measure it at the  
2 same time, without affecting the static angle. The act of bringing the suspension  
3 to its loaded position causes clamping and fixturing to be difficult as well as  
4 forces one to account for a pitch bias, because the loading is not at the suspension  
5 bond pad. In addition, if the loading mechanism is not perfectly centered on the  
6 load beam, the act of loading can cause a roll bias in the angle measurement.

7 In the past, some have measured static angles in the unloaded condition, but  
8 the measurement reference was the plane of the suspension beam and not the  
9 mounting plate plane (actuator arm interface). This reference problem resulted in an  
10 unpredictable bias between the measured static angles and the real static angles.

11 Placing the read/write slider on the suspension is primarily a manually  
12 process wherein pins or cavities in tooling hold each component in alignment. While  
13 the position target is to align the suspension load point to the designed location on  
14 the slider air bearing, tolerances make this a difficult task. U.S. Patent No.  
15 4,866,836 addresses these tolerances by optically aligning the slider body to the  
16 suspension (dimple) load point. This technique alleviates the load point source of  
17 torque variation, but it does not address the torque from suspension, circuit, bond line  
18 parallelism and slider parallelism tolerances.

1           Several techniques have been attempted to "bond out" the static angles from  
2 the suspension and slider (parallelism). These are described in U.S. Patent Nos.  
3 5,608,590; 5,473,488; 5,661,619; 5,729,889 and 5,636,089. These concepts attempt  
4 to counter torque from static angle tolerances by allowing the adhesive to form a  
5 wedge between the slider and suspension bonding surfaces. These techniques do not  
6 address torque from load point tolerances and the adhesive wedge is difficult to  
7 control, at best, thus it does not "bond out" the static angle tolerances.

8           U.S. Patent Nos. 5,198,945 and 5,282,102 teach integrated flexure  
9 suspensions that reduce some load position errors, but do not address torque from  
10 static angle tolerance, bond line parallelism or slider parallelism.

11           U.S. Patent No. 5,682,780 is an example of a suspension adjustment  
12 technology used to decrease some of the static angle variation from the suspension  
13 components, which involves deforming the mechanical suspension. It does not  
14 address load point, bond line parallelism or slider parallelism sources of torque.

15           A technique has been used to measure the torque acting on the slider body  
16 and shift the slider relative to the suspension to minimize the torque during slider  
17 bonding. This technique is shown in U.S. Patent No. 5,371,939. While this  
18 technique adjusts slider position to account for torque from static angles, load point,  
19 and slider parallelism, it requires aligning the slider with the suspension in a loaded

1 position and requires that small actuated fixtures come in contact with the slider  
2 body. Bringing the suspension to the loaded position involves precise clamping and  
3 very controlled distances between that clamp surface and the loading surface. Thus,  
4 inherently, this technique is difficult to automate and achieve high throughput.

5 The foregoing discussion of current head gimbal assembly procedures has  
6 highlighted several of the problems with the current assembly procedures and pointed  
7 out the long-felt but unsatisfied needs of the industry. Thus, there is a need for a  
8 method of only aligning the head termination pads to the interconnect leads rather  
9 than the gimbal load point as well as a need for simplifying the fixturing to reduce  
10 damage to the suspension. Also, there is a need for a fast, automatable method for  
11 performing a dynamic electrical head test before the head is mounted to a suspension.  
12 Yet again, there is a need for a fast, automatable method of mounting a slider without  
13 the use of complicated tools and applying a load, which does not damage the  
14 suspension and accounts for static angle torques. Additionally, there is a need for a  
15 fast, automatable static angle measurement system that does not require loading the  
16 suspension, but uses a predictable and functional reference surface. Finally, there is  
17 a need for a fast, automatable method to align and attach a slider to a suspension,  
18 while accounting for all sources of torque variation.



SUMMARY OF THE INVENTION

1  
2 It is an object of the present invention to provide new and improved apparatus  
3 that is not subject to the foregoing disadvantages.

4 It is another object of the present invention to provide a method for attaching  
5 a head/slider to a circuited gimbal with one or more of the following advantages:  
6 without damaging the suspension; with improved alignment between the termination  
7 pads of the head/slider and the circuited gimbal; with simplified tooling; or with  
8 simplified tooling and improved substrate heating and control.

9 It is still yet another object of the present invention to provide a method for  
10 a dynamic electrical test of the read/write head without the suspension present with  
11 low cost and high throughput, thereby obviating the need to throw away a good  
12 suspension when a given head is found to be rejectable under DET test criteria.

13 It is still a further object of the present invention to attach a  
14 head/slider/circuited gimbal to a suspension and compensate for torque from  
15 suspension, circuited gimbal, bond line, and slider parallelism static angles, as well  
16 as load point.

17 It is another object of the present invention to reduce operator handling and  
18 other sources of ESD or EOS, which could otherwise damage the head element.

1           The present invention provides a method for assembling a head gimbal  
2 assembly useful in a hard disk drive and for testing such an assembly. In a method  
3 in accord with the present invention a head slider is mounted to a circuited gimbal  
4 in an automated assembly machine using an adhesive dispenser to dispense adhesive  
5 on a circuited gimbal, an automated pick and place machine to position a slider  
6 relative to the circuited gimbal, a vision system to precisely locate the slider and  
7 circuited gimbal with respect to each other, and the pick and place machine to place  
8 the slider on the circuited gimbal. The electrical contacts in the slider are then  
9 terminated to the traces or electrical leads of the circuited gimbal using an automated  
10 electrical termination machine.

11           Following termination, the head/slider/circuited gimbal assembly may have  
12 a dynamic electrical test performed on it at a dynamic electrical test station. The  
13 assemblies can be sorted based upon the test results and those that do not meet the  
14 test specifications can be sorted from the assembly process.

15           Following the DET, those assemblies meeting the DET specifications will be  
16 attached to suspensions in an automated assembly apparatus. The assemblies will be  
17 placed in the apparatus and measurements will be made of the suspension static  
18 angles with reference to the load beam and an area near the base plate with an  
19 autocollimator. Adhesive will be dispensed by the automated apparatus onto the

1 suspension while the static angles are measured on the air bearing surface of the  
2 head/slider/circuited gimbal assembly relative to the circuited gimbal body. The air  
3 bearing position relative to the suspension load point will be determined so that the  
4 torque that acts on the air bearing is optimized in pitch and roll directions. The  
5 assembly can then be mounted to the suspension.

6 The foregoing objects of the invention will become apparent to those  
7 skilled in the art when the following detailed description of the invention is read  
8 in conjunction with the accompanying drawings and claims. Throughout the  
9 drawings, like numerals refer to similar or identical parts:

#### 10 BRIEF DESCRIPTION OF THE DRAWINGS

11 Figure 1 illustrates an isometric view of a head slider bond station.

12 Figure 2 illustrates an isometric view of a head slider and bond area  
13 enlarged from Figure 1 to show electrical termination leads.

14 Figure 3 is an isometric view of a head/slider/circuited gimbal during a  
15 ball bond electrical termination process.

16 Figure 4 is an isometric view of a head/slider/circuited gimbal assembly.

17 Figure 5 is a side view of a head/slider/circuited gimbal assembly flying  
18 over a disk connected to a goniometric cradle and stage assembly.

1        Figure 6 is a close up of Figure 7 showing a side view of the vacuum  
2        collet detail.

3        Figure 7 is a close up of Figure 7 showing the slider portion of the  
4        assembly with respect to a spinning disk.

5        Figure 8 is a detailed isometric view of the test pads and contact points  
6        within the vacuum collet.

7        Figure 9 is a sectioned view of a head/slider/circuited gimbal assembly  
8        held in a processing tray.

9        Figure 10 is an isometric view of a static angle measurement for the  
10       head/slider/circuited gimbal in a processing tray.

11       Figure 11 is a section view of a static angle measurement for a suspension  
12       wherein the suspension is picked from a processing tray and rotated with the  
13       collet acting as reference.

14       Figures 12A-12C are end views of a static angle measurement for a  
15       suspension wherein the suspension is picked and rotated to a reference surface  
16       from a processing tray.

17       Figures 13A and 13B are end views of a static angle measurement for a  
18       suspension wherein the suspension is picked and rotated from a processing tray  
19       with the collet acting as reference.

1           Figure 14 is a section view of a static angle measurement for a suspension  
2           wherein the suspension is held in a processing tray and a second measurement  
3           probe provides the reference surface.

4           Figure 15 is an isometric view of an assembled head gimbal assembly.

5           Figure 16 is a front section view of a head gimbal assembly before a  
6           torque management bond.

7           Figure 17 is a histogram representing state of the art torque distributions  
8           without using this invention.

9           Figure 18 is a histogram representing an improved torque distribution  
10          using this invention without directly measuring the suspension load position.

11          Figure 19 is a histogram representing an improved torque distribution  
12          using this invention while directly measuring the suspension load position.

13          Figure 20 is a perspective, exploded view of a suspension and an  
14          interconnect.

15          Figures 21 and 22 are details of the circled area I of the suspension shown  
16          in Figure 1.

#### 17                           **DETAILED DESCRIPTION OF THE INVENTION**

18           A solution to each of the above mentioned problems is a novel process  
19           flow combined with processing methods to accurately attach a read/write

1 head/slider, make the electrical connection, perform a dynamic electrical test on  
2 the head prior to suspension attachment, measure static angles without loading the  
3 suspension and manage the final torque acting on the slider body to assure proper  
4 flying characteristics. This method will first be described generally and then more  
5 specifically to follow.

6 A tray or batch of head sliders are mounted to circuited gimbals in an  
7 automated pick and place machine, utilizing vision, stages, adhesive dispense and  
8 ultra-violet (UV) tacking. Such machines are known in the art and will be  
9 described generally herein. The circuited gimbals are of the type that includes  
10 integral traces, but are not completed suspension assemblies. The sliders are  
11 provided as individual pieces in their own respective package.

12 Once the sliders and circuited gimbals are placed in the assembly  
13 apparatus, adhesive is dispensed on the circuited gimbals and the slider is picked  
14 from its tray with a vacuum collet of the pick and place machine. The slider is  
15 brought to hover over the circuited gimbal. The vision system of the pick and  
16 place machine aligns the air bearing surface to the electrical termination pads of  
17 the circuited gimbal or optical alignment fiducials found on the circuited gimbal  
18 and/or slider, which facilitates predictable electrical termination in the next  
19 operation. The air bearing is not placed relative to a load point, since the

1 suspension is not yet present. Holding of the slider circuited gimbal in this  
2 operation is simple, since it is a flat, predominantly two-dimensional structure.  
3 The slider is brought to the circuited gimbal with a precise and known Z-force  
4 from the Z-stage, providing a very controlled placement. As the slider is held,  
5 UV light may be used to tack cure the adhesive to hold the desired position. The  
6 batch of head/slider/circuited gimbal assemblies can be oven cured off-line.

7 A batch of head/sliders attached to circuited gimbals is brought to an  
8 automated electrical termination machine, such as a gold ball or ultrasonic wedge  
9 bonder. Since the circuited gimbal is predominantly two dimensional and the  
10 head/slider is firmly attached with adhesive, holding the assembly during  
11 electrical termination is very easy. Further, since the suspension is not yet  
12 present, the manufacturer does not need to be concerned about damaging the  
13 suspension with this operation.

14 The electrically terminated head/slider/circuited gimbal assemblies are  
15 brought to an automated DET station with the air bearings facing away from a  
16 vacuum collet pick up. Much like a pick and place machine, a vacuum collet  
17 picks up an individual head/slider/circuited gimbal assembly and brings it in  
18 proximity to a spinning test disk. During the vacuum pick up, a temporary  
19 electrical connection is made. The precise and known force through the z-stage is

1 also the force passing through the slider air bearing. Thus, the slider can fly and  
2 position the head at the proper magnetic spacing without the presence of a  
3 suspension. During this test, numerous sensitivities can be determined on the  
4 individual heads, by varying the load, skew angle, disk speed and so on. Heads  
5 can be sorted into good, marginal and bad bins. Since this test occurs before a  
6 suspension is present, the test allows the assembler to discern head failures due to  
7 the heads and not the suspension. Further, this method enables the assembler to  
8 save a significant cost by not bonding bad head/sliders to good suspensions.

9       Trays of good head/slider/circuited gimbals are next assembled to  
10 suspensions. A pick and place machine with vision, adhesive dispense, a vacuum  
11 collet and UV tack source is used. The suspension static angles are measured  
12 with reference to the beam and an area near the base plate with an autocollimator.  
13 Adhesive is dispensed onto the suspension. On the head/slider/circuited gimbals,  
14 static angles are measured on the air bearing surface relative to the circuited  
15 gimbal body. The pitch and roll stiffnesses of both the suspension and the  
16 circuited gimbals are known via off-line characterization. An algorithm is used to  
17 determine the air bearing position needed relative to the suspension load point,  
18 such that the resultant torque acting on the air bearing is optimized in both pitch  
19 and roll directions. Thus, all sources of static attitude torque from the suspension,



1 static attitude of circuited gimbals, bond line parallelism, or slider parallelism is  
2 compensated for by adjusting the load point during head/slider/circuited gimbal  
3 attachment to the suspension.

4 Traditionally, ESD is a major source for yield loss because, in part, of the  
5 labor intensive nature of the process. During each of the process steps described  
6 above, the head/slider is automatically handled with a pick and place machine,  
7 which greatly reduces the probability of an electrostatic discharge damaging the  
8 sensitive head. Manual handling of the electrostatic dissipative trays occurs only  
9 when the trays are closed.

10 Reference will now be made to the drawings to more fully describe the  
11 foregoing process. Referring now to Figures 1-2, the bonding of the head/slider  
12 100 to the circuited gimbal 102 will now be described. The circuited gimbal 102  
13 includes a head/slider bond tab 104 and a flexible circuit 106, which in turn  
14 comprises a flex circuit body 108 and an interconnect 110. Batches of head/sliders  
15 100 and circuited gimbals 102 will be placed in a pick and place machine (not  
16 shown in all detail). Such a machine may be purchased from Zmation, Inc. of  
17 Portland, Or. Such a machine will typically have ranges of motion in the X,Y,  
18 and Z directions and in an angular direction  $\Theta$  about the Z axis. An adhesive  
19 dispenser will dispense adhesive onto the bonding surface 112 of the head/slider

1 bond tab 104 of the circuited gimbal 102. The pick and place machine will have a  
2 vision system 114 associated therewith, which may be used first to place adhesive  
3 precisely onto the bonding surface 112 and subsequently to align the components  
4 100 and 102 for precision bonding. The volume and/or pattern and/or location of  
5 the adhesive dispense, as well as the type of adhesive(s) (i.e. conductive,  
6 structural, both, etc) may vary dependant on component design.

7 Following the dispensing of the adhesive, the head/slider 100 will be  
8 picked from its place in the tray or batch of head/sliders by a vacuum collet 116  
9 associated with the pick and place machine and brought to hover over the  
10 circuited gimbal bonding surface 112. The vision system 114 will precisely  
11 determine the respective, precise positions of the head/slider 100 and the bonding  
12 surface 112 and particularly the electrical termination pads 118 of the head/slider  
13 bond tab 104 for the read/write leads 120 extending to and from the head/slider  
14 100. That is, the vision system 114 will image the precise positions of the  
15 head/slider 100 and the circuited gimbal 102 or optical targets/fiducials placed  
16 thereon and will locate the components 100, 102 using vision processing  
17 algorithms. The results of the vision processing algorithms will then be used to  
18 direct the various motion stages, typically X,Y, and  $\Theta$  stages, of the vacuum collet  
19 116 attached to the pick and place machine. That is, the results of the vision

1 processing algorithms will be used to position the head/slider directly over the  
2 desired bonding location and to lower the collet 116 and the attached head/slider  
3 100 with a precise and known downwardly directed or Z-force from the Z-stage of  
4 the pick and place machine to which the vacuum collet 116 is attached, onto the  
5 bonding surface 112. Thus, the present invention provides a very controlled  
6 placement of the head/slider 100 so as to precisely align the termination pads 122  
7 of the head/slider 100 with the termination pads 118 of the circuited gimbal 102.  
8 As the head/slider 100 is held in bonding position against the bonding surface  
9 112, UV light may be used to tack cure the adhesive to hold the head/slider 100 in  
10 the desired position relative to the bonding surface 112. This process will be  
11 repeated until the entire batch or tray of adhesions of head/sliders 100 to circuited  
12 gimbals 102 is completed, forming a tray or batch of head/slider/circuited gimbal  
13 assemblies (HSCG). The completed batch of HSCG assemblies can be oven  
14 cured off-line.

15 It will be understood that using the aforescribed method of assembling  
16 the head/slider 100 to the circuited gimbal 102 results in the air bearing not being  
17 placed relative to the load point, since the suspension is not yet present.

18 Attachment of the head/slider 100 to a circuited gimbal 102 presents several  
19 advantages over the current assembly procedure of attachment of the head/slider

10073600-SEP10E  
1 100 to a completed suspension/flex circuit assembly. First, the attachment  
2 operation is simplified because the circuited gimbal is a relatively flat,  
3 substantially two dimensional structure. The flex circuit 106 typically comprises  
4 a base polyimide material 124 with this electrical leads laid thereon. Such a flex  
5 circuit usually includes a cover material also made out of polyimide. Thus, the  
6 flex circuit is substantially planar with a small thickness. Consequently, the  
7 head/slider 100 can be pushed flat against the circuited gimbal with the lowering  
8 of the collet 116 without worry about adversely affecting static attitude of the  
9 completed suspension assembly.

10 While the above description utilized X, Y, Z motion on the vacuum collet,  
11 it is anticipated that the tray holding the circuited gimbal could be moved with  
12 any combination of said stages rather than having all degrees of freedom attached  
13 to the collet.

14 Following complete curing of the adhesive bond between the head/slider  
15 100 and the circuited gimbal 102, the terminations 118, 122 will be electrically  
16 connected in a process known as termination. Referring now to Figure 3, the  
17 process will be described. Termination will occur in an automated termination  
18 machine, partially shown in the Figure, which will include mounted on the  
19 appropriate stages for motion in desired directions a loading station (not shown

1 for purposes of clarity), a bondhead 130, clamp 132, and a vision system 134.  
2 Such a machine may be purchased from F&K Delvotek, Inc. of Ottobrunn,  
3 Germany. The bondhead 130 is designed for either ball bond or tab bonding, the  
4 particular type of bonding used being dependent upon the product configuration  
5 being either a ball bond or a direct lead. The loading station will preferably be an  
6 X and Y stage. The bondhead and vision system are mounted on an X,Y, and Z  
7 stage. The clamp 132 can be a part of or independent from the stages.

8 Termination will begin with the loading of a tray 136 or batch of HSCG  
9 assemblies 138 into the termination machine. Once loaded, the vision system 134  
10 will individually locate either the head/slider edges, head pads, head/slider air  
11 bearing surface or the circuited gimbal fiducials 139 or any other predictable  
12 surface geometry thereof to properly locate the termination targets, termination  
13 pads 122. Once the HSCG has been optically located, the HSCG assembly will  
14 be clamped by clamp 132 and held gently in position to withstand the lateral  
15 forces of bonding. Using the information provided by the vision system 134 to  
16 precisely locate the termination pads 122, the bondhead 130 will be moved into  
17 position over each termination target and will bond the termination pads 122 to  
18 the leads 120 with a material such as gold, shown in the shape of a gold ball 140  
19 in the Figure. Once the termination of an HSCG assembly is completed, the

1. HSCG assembly will be unclamped and the bondhead will be positioned over the  
2 next part to repeat the process until the entire tray of HSCG assemblies is  
3 terminated.

4 If desired, the tray 136, fixture, or other surface upon which the HSCG  
5 assemblies are presented for termination can be constructed such that the HSCG  
6 can be heated to facilitate termination. In addition, the bondhead 130 or part tray  
7 136 may be mounted at an angle to promote optimal scrubbing of both the leads  
8 and slider pads during bonding.

9 The advantages over conventional methods of this automated method for  
10 terminating leads to sliders without the presence of suspensions are numerous.  
11 First, since the suspension is not present during this operation and vision is  
12 utilized, fixturing is simplified and thus provides flexibility, low maintenance, and  
13 low cost. Second, better clamping and substrate - that is, tray or fixture - heating  
14 will promote improved bonding quality. Third, as with the process of bonding the  
15 head/slider 100 to the circuited gimbal 102, because of the flat, predominately two  
16 dimensional structure of the HSCG assembly, the tooling needed to hold the  
17 HSCG assemblies can be flat and require only the use of rough locating features.  
18 This significantly reduces the complexity of the tooling, increases its  
19 compatibility with other part configurations, and enables bonding to occur with no

1 static attitude damage. Fourth, the use of a vision system to locate the termination  
2 targets will guarantee accurate bond placement. Accurate termination placement  
3 is aided by the accurate lead to pad alignment already performed in the previous  
4 process of bonding the head/slider to circuited gimbal. In conventional slider  
5 attachment processes, the main objective is to align the head/slider with the  
6 suspension's load point or dimple. This conventional method, however, does not  
7 guarantee good pad to lead alignment, which may cause poor termination. In the  
8 inventive process, head/slider termination is done independent of the presence of a  
9 suspension. Therefore, the main objective is pad to lead alignment and; hence,  
10 good termination. The alignment of the head/slider to the suspension occurs at a  
11 separate post termination process: Torque Management. Fifth, because this is an  
12 automated process, the risks of contamination and ESD and EOS are minimized.  
13 Finally, if a reject occurs, scrap cost is less because a suspension is not wasted.  
14 Cost savings also result from a reduction in cycle time and direct labor costs.

15 While the present description uses ball bonding as an example, it is  
16 contemplated that other electrical connection methods can be used without  
17 deviating from the spirit of the present invention.

18 Following termination, the electrical properties of the HSCG assembly can  
19 be determined using a DET process. The DET is a quality control test employed

1 to determine whether the electrical characteristics of the head and circuit are  
2 acceptable. This test process will be described with respect to Figures 4-8. In the  
3 preferred embodiment, the DET is performed in an automated fashion by a  
4 dynamic electrical test machine, or DETM 150.

5 In general, and as is known in the art, the DETM consists of the following  
6 principle components: 1) an X, Y, Z, and  $\Theta$  motorized gantry system, 2) a pattern  
7 recognition system, 3) a spinstand mounted to a goniometric cradle and a nano X-  
8 Y stage, 4) the test electronics, and 5) an instrumented vacuum collet. Again,  
9 because such machines are known in the art, they will only be briefly described.  
10 Such a machine may be purchased from Zmation, Inc. of Portland, Oregon.

11 The instrumented vacuum collet 152 is mounted to the Z-theta motor, and  
12 thus has X, Y, Z, and theta range of motion. The vacuum collet's contact probes  
13 154 are electrically connected to a preamplifier and the associated instrumentation  
14 required for head characterization. The camera and optics for the pattern  
15 recognition system are mounted to the gantry head, and have X, and Y motion.  
16 The spin stand, nano-stage and goniometric cradle are mounted on the DETM  
17 within the range of motion of the gantry head. The HSCG assemblies are  
18 orientated in the DETM such that the air bearing surfaces 148 (best seen in Figure  
19 2) of the slider bodies are facing away from the vacuum collet.



1 To perform a dynamic electrical test on a HSCG assembly 138, the DETM  
2 first positions the optics for the pattern recognition system above a HSCG  
3 assembly 138. The pattern recognition system accurately determines the position  
4 information of the HSCG assembly 138 so that the instrumented vacuum collet  
5 150 can be aligned relative thereto. Once aligned, the vacuum collet 150 is  
6 lowered until the probes 154 contacts the test pads 156 (Figure 8) of the HSCG  
7 assembly, which are electrically connected to the leads 118. Vacuum is applied  
8 through the vacuum ports in the collet, securing both the test pads 156 and body  
9 portions of the HSCG assembly to the instrumented collet. In doing so, the  
10 vacuum collet's contact probes 154 each engage with their respective test pads  
11 156 on the HSCG assembly to create an electrically conductive interface. As a  
12 result, an electrical path is established between the head and test electronics on the  
13 DETM. The HSCG assembly 138 is then positioned above the spinstand 158.

14 The gantry's Z-stage actuator is typically a voice coil motor. The current  
15 draw and stroke position of the Z-actuator strongly correlates to the force applied  
16 by the actuator arm of the hard disk drive. The Z-axis actuator lowers the HSCG  
17 assembly so that the slider's air bearing surfaces (ABS) begins to fly above the  
18 spinstand's spinning media disk 160. The disk 160 is rotated at the proper speed  
19 by a motor 162 attached to the disk by a spindle 164. In order for the slider to

1 "fly" correctly in relation to the disk 160, the proper downward force must be  
2 applied to the slider. The current draw and stroke position information of the Z-  
3 axis actuator are monitored to ensure that the proper amount of force is being  
4 applied to the slider via the collet and gimbal so as to ensure the desired test  
5 conditions are being met.

6 As the Z-actuator applies a downward force on the body of the HSCG  
7 assembly, an equal and opposite lift force is applied to the ABS of the slider by  
8 the passage of air between the slider ABS 148 and the media disk 160. Because  
9 the two equal and opposite forces acting on the HSCG assembly 138 are  
10 substantially off-axis, the resulting moment can cause the gimbal to deflect out of  
11 plane. This out of plane deflection results in a reaction torque load that is applied  
12 by the HSCG assembly at the slider's ABS 148 and at the vacuum collet interface.  
13 The torque applied by the slider's ABS can have a significant affect on the flight  
14 characteristics of the ABS 148 over the spinning media. In order to obtain the  
15 desired flight characteristics, the goniometric cradle 166 positions the spinning  
16 media disk 160 at a substantially non-horizontal angle such that the torque applied  
17 by the slider's ABS 148 is minimized.

18 Once the HSCG assembly 138 is positioned over the spindstand's spinning  
19 media disk 160 and the slider's ABS 148 is in proper flight, the test electronics

1 associated with the DETM begin to electronically characterize the head  
2 parameters. The nano-X-Y stage 168 is used to position the spinstand 158 so that  
3 the location of the head /slider 100 relative to the spinstand's spinning media disk  
4 160 can be manipulated to correct for track positioning. In addition, this allows  
5 the test to be performed at any radial location on the media disk 160, from its  
6 inner diameter to its outer diameter. The nano X-Y stage 168 can also be used to  
7 manipulate the skew angle of the HSCG assembly 138 during testing.

8       Once the head's parametric characterization is complete, the HSCG  
9 assembly 138 is returned to its initial location, and the test is repeated on the next  
10 HSCG assembly.

11       The DETM can also be used to perform further characterizations on the  
12 HSCG assemblies 138. For example, by varying the downward force applied by  
13 the z-actuator, the angle 170 of the media disk with the goniometric cradle, the  
14 skew angle, the radial location of the head with the nano x-y stage, and/or the  
15 rotational speed of the media a head parameter sensitivity analysis can be  
16 performed.

17       Once the DET has been completed on a batch of HSCG assemblies, they  
18 are ready for a static angle measurement. Determination of the static angles on  
19 the circuited gimbal may be made using several clamping schemes and various

1 non-contact measurement systems. In the preferred embodiment, the  
2 measurements will be conducted using an autocollimator positioned over the part  
3 in its processing tray 180, shown schematically in cross section in Figure 9. The  
4 tray will provide the clamping surface 182 for the circuited gimbal by means of  
5 vacuum chamber 184 connected to a vacuum port 186 connected to a vacuum  
6 source, thus providing a suction to hold the HSCG assembly 138 and a controlled  
7 datum or zero reference 188. The autocollimator 190 will be positioned, during  
8 measurement, over the ABS 148 of the head/slider 100 as shown in Figure 10.  
9 The measurement, then, provides relative static angles between the controlled  
10 datum and the air bearing surface. After the measurement is made, the static  
11 angle information for the HSCG assembly is stored for later use and the  
12 autocollimator 190 moves, via an X-Y stage, to the next part for measurement and  
13 data storage. Autocollimation is a well known technique for measuring static  
14 angles by means of a collimated beam of light 192, as shown by "Static Attitude  
15 Test Probe Operator's Guide," published by Wyko Corporation, a manufacturer of  
16 autocollimators.

17 In alternate embodiments, other non-contact means of angle measurement  
18 may be used, including, but not limited to: specular laser triangulation, diffuse  
19 laser triangulation, monochromatic light interferometry and white light.

1 interferometry. The circuited gimbal may also be measured using a vacuum collet  
2 as a clamping surface. Similarly, the static angles may be measured on surfaces  
3 other than the air-bearing surface of the slider, such as the various areas on the  
4 circuited gimbal near or behind the slider. Any of the aforementioned  
5 embodiments for static angle measurements of circuited gimbals may be carried  
6 out in combination with other processes described herein or as a separate process.

7 Having determined the static angle measurements of the ABS 148, the  
8 static angles of the suspensions must now be made. Similar to the measurement  
9 of static angles on circuited gimbals, the determination of the static angles of the  
10 suspension may be made using several clamping schemes and various non-contact  
11 measurement systems.

12 In the preferred embodiment, the measurements will be conducted using  
13 an autocollimator 200 mounted horizontally. Suspensions 202 would be  
14 sequentially picked from a suspension tray 204, measured and replaced in the tray.  
15 The suspensions are picked up from the tray 204 using a vacuum collet 206,  
16 which clamps on a datum surface of the suspension. The collet is configured such  
17 that it allows the suspension 202 to be swung vertically from the pick position 208  
18 to a reference position 210 about a rotation point 212 and into the view of the  
19 autocollimator 200 to a measurement position 214 where the measurement is

1 taken on the gimbal 218 of the suspension 200 using a collimated light beam 216.  
2 On parts that do not have a gimbal surface, the measurement will be taken on the  
3 suspension beam at a location closest to its tip and where the circuited gimbal will  
4 ultimately be secured. The measurement provides relative static angles between  
5 the controlled datum and the gimbal or load beam measurements.

6 Measurement information for the suspension's static angles is stored for  
7 later use. The same collet 206 replaces the suspension 202 into the tray 204  
8 before moving, via X-Y stages, to the next part to repeat the process.

9 Other embodiments to achieve a similar result may be pursued if higher  
10 accuracy is required. Referring to Figures 12A-12C, such embodiments may  
11 include picking the suspension 202 from the tray 204 as above using a collet 220,  
12 except in a linear motion. The collet 220 then rotates the suspension 202 such  
13 that its base 222 is placed into a clamp 224 while the collet 220 is released for  
14 more precise datum pickup and such that the opposite end - the gimbal - is in  
15 view of the autocollimator 226. After measurement, the collet 220 will again pick  
16 the suspension 202 while held by the clamp 224, the clamp 224 will release, and  
17 the collet 220 and suspension 202 will rotate to their original position to then  
18 lower the suspension 202 back into the tray.

1 A similar embodiment would have a similar pick, but no rotation for  
2 clamping and measurement, rather, the X-Y stage would move the suspension to a  
3 remote clamp and autocollimator for measurement.

4 In either of the two aforementioned embodiments, the suspension 202 may  
5 be picked up by the vacuum collet either on the main section of the suspension  
6 beam or on the base itself. These embodiments are also potentially more  
7 expensive than other embodiments since the tooling costs of precise datum  
8 clamping are high.

9 Two other embodiments, provide linear vertical collet pick up of the  
10 suspension by the base. In one embodiment shown in Figure 13A, the collet 240  
11 lifts and then rotates the suspension 202 horizontally, over a mirror 242 allowing  
12 the autocollimator 244 a view of the measurement area as seen in Figure 13B.  
13 Thus, in this embodiment, the autocollimator 244 emits a beam of collimated light  
14 246 that reflects off the mirror 242 onto the controlled datum, which is reflected  
15 back to the mirror 242 and to the autocollimator 244 for a measurement.

16 In still another embodiment, the collet moves via the X-Y stage to a  
17 remote measurement location for the autocollimator to obtain a view of the  
18 measurement area on the suspension.

1 Still another embodiment allows for high speed measurements by not  
2 contacting the suspensions at all as seen in Figure 14. In this embodiment, one or  
3 two autocollimators 250 are positioned over a part, here shown as suspension 202  
4 though it could also be HSCG 138, using an X-Y stage. Either the parts or the  
5 autocollimator(s) 250 is moved. The part is clamped by vacuum in the processing  
6 tray 204. Simultaneous or sequential measurements are taken of the gimbal 218  
7 or the loadbeam 252 and the base 256. This approach will result in relative  
8 measurements between the gimbal 218 or beam 252 and a surface that is not  
9 functional in the drive and therefore, this approach may not be as accurate as other  
10 embodiments.

11 While the above description utilized measurements at certain points on the  
12 various components, it is anticipated that other points may be taken along the  
13 length of any components.

14 In variations to the aforementioned embodiments, other non-contact means  
15 of angle measurement may be used, including, but not limited to: specular laser  
16 triangulation, diffuse laser triangulation, monochromatic light interferometry and  
17 white light interferometry.



1 Any of the aforementioned embodiments for static angle measurements of  
2 suspensions may be carried out in combination with other processes described  
3 herein or as a separate process.

4 Another important factor in the assembly and operation of a hard disk  
5 drive is management of the torque. The torque management process can be  
6 described sequentially in the preferred method as follows: a) The static angles,  
7 measured in a previous step of the process, for the suspension assemblies 202 are  
8 electronically loaded into the torque management computer. This data is used in  
9 conjunction with other entered data such as the pitch and roll stiffness of the  
10 suspension assemblies 202 to calculate, among other things, the pitch and roll  
11 torques of the suspension assemblies 202. b) Adhesive is dispensed onto the  
12 suspension assembly c) The static angles of the HSCG assembly 138 are now  
13 measured if not measured previously. These angle measurements are taken with  
14 respect to the body 108 of the HSCG assembly 138. The actual angles are  
15 measured on the ABS of the head/slider 100. The pitch and roll stiffness of the  
16 circuited gimbal 100 are known via off-line characterization and have previously  
17 been loaded into a torque management computer associated with the torque  
18 management station. d) With the static angles of the suspension assembly 202  
19 and the HSCG assembly 138 now known, as well as the stiffness information, the

1 required position of the HSCG assembly 138 relative to the suspension assembly  
2 202 can now be calculated such that the resultant torque of the entire head gimbal  
3 assembly acting on the ABS is optimized in both pitch 300 and roll 302.

4 The following method for calculating the offset "X" required to optimize  
5 roll torque is shown as an example. The method for pitch torque is essentially the  
6 same. In addition, the method may vary slightly depending on such factors as  
7 methods of angle measurements and datum's for such.

8 Figure 16 should be referred to for the following example of a calculation  
9 of roll torque. Figure 16 is a cross section through a typical suspension 202 and  
10 HSCG assembly prior to attachment. Thus, the figure shows a suspension load  
11 beam 252 and the suspension flexure 306 disposed below an HSCG assembly 138  
12 including the head/slider 100, the flex circuit 202, and an adhesive 308 bonding  
13 the two together. In doing so, it will be understood that the following symbols  
14 have the following meanings.

15 X = Offset (reference numeral 310 in Figure 16)

16  $\Theta$  = Angle

17 k = stiffness

18 M = Moment (Torque)

1 F = Force (i.e.  $F_{\text{Gram}}$  = Gram Load) (reference numeral 312 in Figure 16)

2 The components of the roll torque of the circuited gimbal are as follows:

- 3 1. The roll torque of the flex circuit. This is the product of the static  
4 roll angle of the flex circuit gimbal (relative to the flex circuit  
5 body) and the flex circuit roll stiffness.  
6 2. The roll angle of the slider relative to the flex circuit gimbal. This  
7 is usually set by the parallelism of the bond line between the slider  
8 and the bonding surface and the ABS.

9 Thus the roll torque of the circuited gimbal,  $\sum M_{\text{Circuited Gimbal}}$  ((reference numeral  
10 314 in Figure 16) is given by:

11 
$$\sum M_{\text{Circuited Gimbal}} = \Theta_{\text{Circuited Gimbal}} \times k_{\text{Circuited Gimbal}}$$

12 The angle of the circuited gimbals is preferably measured on the ABS (Air  
13 Bearing Surface).

14 The components of the roll torque of the suspension assembly are as  
15 follows:

1. The roll torque of the suspension flexure. This is the product of the static roll angle of the suspension flexure (relative to clamp surface of suspension assembly) and the flexure roll stiffness.
2. The product of the gram load and the load point shift ( $X_0$ )(if any).

Thus the roll torque of the suspension assembly  $\sum M_{\text{SuspensionAssembly}}$  (reference numeral 316 in Figure 16) is:

$$\sum M_{\text{SuspensionAssembly}} = \Theta_{\text{SuspensionFlexure}} * k_{\text{SuspensionFlexure}} + F_{\text{Gram}} * X_0$$

To calculate "X", a nominal roll torque is assumed. Thus:

$$\text{Nominal Roll Torque } (M_{\text{Head gimbal assembly-Roll}}) = 0.00 \text{ uNm.}$$

$$\sum M_{\text{HeadGimbalAssembly}} = M_{\text{CircuitedGimbal}} + M_{\text{SuspensionAssembly}} + M_{\text{torqueManagement}} = 0$$

$M_{\text{Circuited Gimbal}}$  and  $M_{\text{Suspension Assembly}}$  have been previously defined.

$$M_{\text{TorqueMgmt}} = F_{\text{Gram}} * X$$

1 Solving the equation for the offset X yields:

2 
$$X = -(\Theta_{\text{Circuited Gimbal}} * k_{\text{Circuited Gimbal}} + \Theta_{\text{Suspension Flexure}} * k_{\text{Suspension Flexure}}) / F_{\text{Gram}} - X_0$$

3 where  $X_0$  is the load point shift with respect to the suspension dimple and  
4 suspension flexure.

5 If the gimbal is entirely integrated into the flex circuit, then  $X_0$  is 0.0. If  
6 there is a flexure already attached to the suspension, the load point shift,  $X_0$ ,  
7 should be measured. This may be done with the same vision system that is being  
8 used to precisely align the two components once X is calculated. If the dimple is  
9 an etched tower, then etched fiducials in the suspension assembly can be used to  
10 extrapolate the location of the dimple (since it may be covered up by the flexure).  
11 If the dimple is a formed dimple, then suspension load point tolerances must be  
12 precisely and accurately controlled at the suspension manufacturer (due to the fact  
13 that the load point may not be able to be measured with the vision system). There  
14 will still be some improvement in final fly height with this process, nominal and  
15 distribution size, however it may not be as significant as a product with an etched  
16 dimple or "flex as gimbal".

1 Referring now to Figures 20, 21 and 22, a flex circuit and suspension are  
2 shown in an exploded view relative to each other without the head slider for  
3 purposes of clarity and to more fully illustrate the components upon which the  
4 present invention is practiced. Figures 21 and 22 are detailed views of a portion  
5 of Figure 20.

6 Figure 20 illustrates several components including a suspension A and a  
7 flexible circuit B. It will be understood that the actual physical structures of these  
8 components may vary in configuration depending upon the particular disk drive  
9 manufacturer and that the assembly shown in Figure 20 is meant to be illustrative  
10 of the prior art only. Typically, the suspension A will include a base plate C, a  
11 radius (spring region) D, and a load beam E. Typically the load beam E is bent in  
12 such a way that it causes a spring force, normal to the media disk, to act on the  
13 read/write head in operation. This spring force is counteracted by the lift forces  
14 that result from the read/write head's flight over the spinning media disk. The  
15 load beam E is usually bent near the baseplate C of the head suspension assembly.

16 A typical suspension A will also include a gimbal F having a gimbal load  
17 point G, which is best seen in the detail I shown in Figures 21 and 22. At least  
18 one tooling aperture H may be included. The suspension A may further include

1 an opening or hole J extending through the base plate C and load beam E and a  
2 surrounding collar K.

3 A flex circuit B may include a base, which may be a synthetic material  
4 such as a polyimide, that typically supports a plurality of electrical traces or leads  
5 of the flex circuit. The flex circuit B may also include a polymeric cover layer  
6 that encapsulates selected areas of the electrical traces or leads. Referring briefly  
7 to Figure 20 again, it will be observed that the flex circuit B includes a suspension  
8 portion L and an interconnect portion M.

9 The read/write head that is mounted on the head suspension assembly is  
10 mounted to the gimbal F.

11 Structurally, suspensions such as that shown in the Figures have the base  
12 plate C and gimbal F welded to the load beam as indicated by weld points N. The  
13 flex circuit B is in turn adhesively attached to the suspension A

14 Referring now to Figure 15, the precise positioning of the HSCG assembly  
15 138 relative to the suspension assembly 202 is accomplished in an automated  
16 assembly machine by capturing image(s) of the HSCG assembly 138 and the  
17 suspension assembly 202, usually using optical targets/fiducials placed on one or  
18 both of the assemblies, with a vision camera 320 and using vision processing  
19 algorithms to direct the X,Y, and theta stages to which the vacuum collet 322 is

1 attached (via the z stage) to align the HSCG assembly 138 to the suspension  
2 assembly 202. With the precise positioning of the HSCG assembly 138 relative to  
3 the suspension assembly 202 now complete, the two assemblies are now bonded  
4 together. The HSCG assembly 138 is lowered to the suspension assembly 202  
5 with a precise and known z-force from the z-stage to which the vacuum collet 324  
6 is attached, providing a very controlled placement. As the HSCG assembly is  
7 held in place by the collet 324, UV light may be used to tack cure the adhesive to  
8 hold the desired position producing the head gimbal assembly. The batch of head  
9 gimbal assembly assemblies can be oven cured off-line. Following curing, the  
10 static angle of the bonded head gimbal assembly 326 can then be measured in  
11 order to determine if the calculation and/or placement of the slider-circuited  
12 gimbal assembly 138 to the suspension assembly 202 was successful in  
13 optimizing the resulting pitch and roll torques of the final head gimbal assembly.  
14 This information can be used to optimized the process, either automatically or  
15 manually. Additionally, the final torque can be measured as an audit for process  
16 feedback.

17 While the above description utilized X, Y, Z motion on the vacuum collet,  
18 it is anticipated that the tray could be moved with any combination of said stages  
19 rather than having all degrees of freedom attached to the collet.



1           The main benefit of the above-described process is to minimize torque  
2 variation for improved flying capabilities. The following example shows an  
3 improvement simulation model for a 3 gram head gimbal assembly. The nominal  
4 and 3 sigma variation assumptions for the model variables are as follows:

5           Suspension stiffness 1  $\mu\text{Nm/deg}$ ,  $\pm 0.25$   
6           Suspension static attitude 0 deg,  $\pm 0.75$   
7           Circuited gimbal stiffness 0.4  $\mu\text{Nm/deg}$ ,  $\pm 0.15$   
8           Circuited gimbal static attitude 0 deg,  $\pm 1.5$   
9           Gram 3g  $\pm 0.30$   
10          Load point 0  $\mu\text{m}$ ,  $\pm 30$

11          The model was generated using 100 random data points normally  
12 distributed within the assumed nominal  $\pm 3$  sigma limits of each variable listed  
13 above. Assuming a torque tolerance of 2  $\mu\text{Nm}$  ( $\pm 1\mu\text{Nm}$ ), Figure 17 shows a  
14 torque histogram capability for today's standard, state of the art, process (sigma =  
15 .63  $\mu\text{Nm}$ ). Figure 18 shows a 49% reduction in variation (.32  $\mu\text{Nm}$  sigma) when  
16 the static angles of the suspension and circuited gimbal are taken into account for  
17 shifting the load point position to compensate the torque using the equation above  
18 to calculate the offset X. The variation is further reduced by 75% (.16  $\mu\text{Nm}$   
19 sigma) if load point measurement is improved from  $\pm 30\mu\text{m}$  to  $\pm 15\mu\text{m}$  as seen  
20 Figure 19.

1 In the standard process of attaching the slider to the suspension, the datum  
2 features, namely the boss hole and tooling hole, of the suspension are used to  
3 predict the load point or dimple position. This method can yield a +/- 30µm error  
4 in position. It's expected that this error can be cut in half (to +/- 15µm) if  
5 suspension fiducials are utilized to optically locate the dimple. Furthermore, if a  
6 flexible circuit gimbal is utilized, meaning no stainless steel flexure is present,  
7 vision can be used to locate the dimple directly, whether it be a formed dimple or  
8 etched tower in the load beam, to further reduce the dimple position error.

9 While there may be additional steps in a head gimbal assembly process, such  
10 as cleaning, encapsulation, fly height measurement and others, the present disclosure  
11 only discusses process methods and techniques pertinent to the present invention.

12 While the above advantages are clearly present, other advantages are clearly  
13 anticipated. The preferred embodiments have been disclosed, but others are  
14 envisioned within the general scope of the inventions described herein.

15 he present invention having thus been described, other modifications, alterations, or  
16 substitutions may now suggest themselves to those skilled in the art, all of which are  
17 within the spirit and scope of the present invention. It is therefore intended that the  
18 present invention be limited only by the scope of the attached claims below.

19 WHAT IS CLAIMED IS: